# PROPERTIES OF Y<sub>2</sub>O<sub>3</sub> THIN FILMS APPLICABLE IN MICRO-ELECTROCHEMICAL CELLS

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This work deals with selected mechanical and electrical properties of thin films prepared by planar RF diode sputtering for application in micro-electrochemical biosensors. The properties of  $Y_2O_3$  thin films prepared by RF sputtering are comparable with published data of bulk and  $Y_2O_3$  films. They are suitable for an insulation in the vertically arranged micro-electrochemical cell.

K e y w o r d s: sputtering, micro-electrochemical sensor, interdigitated array of electrodes, insulating yttrium oxide thin film

## **1 INTRODUCTION**

Microelectrodes play a very important role in advanced electrochemical microsensors. Thin films are able to create "the bridge" between macrosystems and microsystems down to molecular systems, *ie*, the research and development of advanced microelectrochemical sensors cannot endure without the utilization of thin film technology. Thin film microelectrodes serve as a base array of electrochemical cells (working/auxiliary Pt, Au, C, reference Ag/AgCl electrodes in compact, microdisk or interdigitated array forms). Their use offers advantages such as diffusion-controlled currents, low charging currents, and reduced solution resistance effects.

The closely spaced interdigitated array (IDA) of electrodes (the width of microelectrode/gap is in  $\mu$ m/sub $\mu$ -m

range) has found a very favourable application in voltametric sensors. When both reduction and oxidation potential is applied to IDA pairs, the effect of redox recycling and high collection efficiency are observed. That specific electrochemical behaviour of IDA revealed a sufficient overlapping of the diffusion layers of the adjacent electrodes causing high current amplification, ie, a significant lowering of the detection limit of the sensor [1].

The thin-film cell consisted of vertically arranged IDA electrodes with a continuous Pt-film basis and an insulation layer, eg, Y<sub>2</sub>O<sub>3</sub> in the middle separating the upper Pt - or Au - IDA electrodes, see Fig. 1. In this arrangement there are IDA with fingers of lengths of 400  $\mu$ m, finger/gap widths of 10/10  $\mu$ m, 5/5  $\mu$ m, 5/3  $\mu$ m. The gap between the bottom and upper microelectrodes is de-

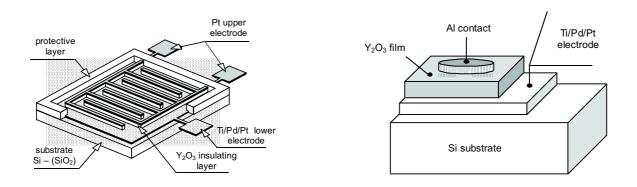


Fig. 1. The thin-film cell consisting of vertically arranged IDA Fig. 2. Arrangement of thin film structures for electrical measureelectrodes ments

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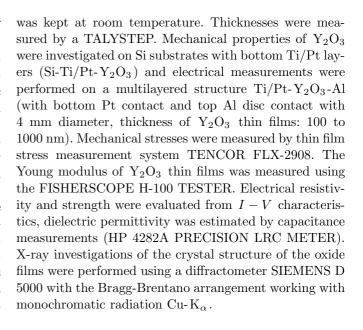
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termined by the thickness of the  $Y_2O_3$  insulating layer (from 0.2 to 1  $\mu$ m).

Therefore the separating insulating layer should satisfy several important requirements: high electric resistivity and strength, low leakage current and dielectric losses, good mechanical properties such as high strength and stability, low intrinsic stress and plastic deformation. Bulk Y<sub>2</sub>O<sub>3</sub> has high values of electrical resistivity, dielectric permittivity, and electric strength, it also has low dielectric losses and good transparency in a wide spectral range with little light diffusion. Its mechanical strength, radiation resistance and high temperature must also be mentioned. Due to these properties,  $Y_2O_3$  is a prospective material for antireflecting and protective coating, interference mirrors and for manufacturing passive components and dielectric layers in multilevel integrated circuits [2]. Vapour deposited and sputtered  $Y_2O_3$  films exhibit desired properties: resistivity  $10^{11} - 10^{12} \Omega m$ , electric intensity  $10^8 - 10^9$  V/m, relative dielectric permittivity 11 - 15, loss tangent  $\delta = 0.01 - 0.03$ , melting point 2430 K, Young modulus 150 GPa, Poisson ratio 0.298, thermal expansion coefficient  $8 \times 10^{-6}$  /K, [2,5,6,7,9]. The aim of this work was optimization of the sputtering technology to get  $Y_2O_3$  films with suitable electrical and mechanical properties.

#### 2 EXPERIMENTAL PART

A planar RF sputtering unit 2400/8L (Perkin-Elmer) was used for the preparation of all the films on Si substrates. The targets of 20 cm in diameter were utilized: metallic Ti (99.9%), Pd (99.9%), Pt (99.9%) and ceramic  $Y_2O_3$  (99.9%). The thickness of the adhesion Ti layer was 50 nm, the barrier Pd layer 50 nm and of the Pt layer 170 nm. The sputtering chamber was pumped down to  $2 \times 10^{-5}$  Pa before admission of the sputtering gas Ar (99.999%), and a total gas pressure of 1.3 Pa was kept constant. Parameters of sputtering of  $Y_2O_3$  films: RF power 800 W, mean induced target DC voltage -900 V and deposition rate 9.5 nm/min, the substrate holder



### **3 RESULTS AND DISCUSSION**

## 3.1 Mechanical properties of $Y_2O_3$ thin films

The mechanical behaviour of thin films is quite different from that of bulk material and is very much governed by the microstructure, impurity and imperfection content which in turn governs the residual stress in the film. As the film gets thicker, the residual stress level decreases and the mechanical properties are very similar to those of thick films or bulk condensates [3].

Thin films deposited by sputtering have usually compressive stresses. This phenomenon is explained by atomic peening [4] in which high energy particles are reflected from the target and bombard the growing films. The intrinsic stress was affected by deposition conditions such as the working pressure.

The total stress  $\delta_{\text{total}}$  of a film consists of two terms [5]

$$\delta_{\text{total}} = \delta_{\text{intrinsic}} + \delta_{\text{thermal}} \tag{1}$$

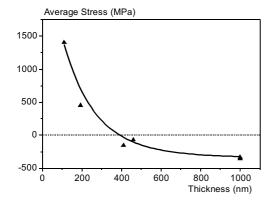


Fig. 3. Dependence of stress on thickness of  $Y_2 O_3$  film

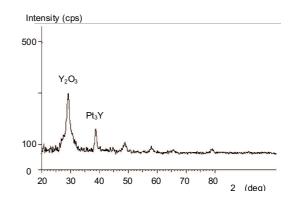


Fig. 4. X-ray investigation of the crystal structure of the samples

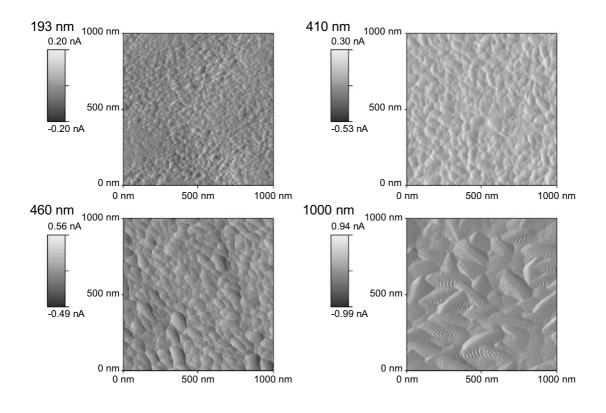


Fig. 5. Surface of  $Y_2O_3$  thin film measured by AFM

were  $\delta_{\text{intrinsic}}$  is the intrinsic stress and  $\delta_{\text{thermal}}$  is the thermal stress. The measured total stress in the thin film is calculated from

$$\delta_{\text{total}} = \frac{Rh^2}{(1-\nu)6Rt} \tag{2}$$

where  $E/(1 - \nu)$  is the biaxial elastic modulus of the substrate, h is the substrate thickness and t is the film thickness. The effective radius is calculated from

$$\frac{1}{R} = \frac{1}{R_1} + \frac{1}{R_2} \tag{3}$$

where  $R_1$  is the initial substrate radius of curvature (Si-Ti/Pd/Pt) and  $R_2$  the new radius after Y<sub>2</sub>O<sub>3</sub> film is deposition. The thermal stress is expressed by

$$\delta_{\text{thermal}} = \frac{E_f(\alpha_s - \alpha_f)\Delta T}{1 - \nu_f} \tag{4}$$

were  $E_f$  is the Young modulus for the film,  $\alpha_s$  and  $\alpha_f$ are thermal expansion coefficients of the substrate and the film, respectively,  $\Delta T$  is the difference between the deposition temperature and the temperature at which the stress has been measured and  $\nu_f$  is the Poisson ratio of the film. The Young modulus characterizes the elastic properties of thin films. For the determination of the Young modulus of the films a method of measuring the hardness under load was used following the procedure described in [6]. The Young modulus of Y<sub>2</sub>O<sub>3</sub> thin films was measured using the device FISHERSCOPE H-100. The measured values of the Young moduli are in agreement with published values [7]. The measured Young moduli were in the range of 150 to 170 GPa. The calculated thermal stress ( $T_{\rm dep} = 300 \,^{\circ}{\rm C}$ ,  $T_{\rm measure} = 20 \,^{\circ}{\rm C}$ ,  $\nu_f = 0.298$ ,  $\alpha_f = 8 \times 10^{-6} / \,^{\circ}{\rm C}$ ,  $\alpha_s = 9 \times 10^{-6} / \,^{\circ}{\rm C}$  [8]) is approximately 60 MPa, which is tensile.

Table 1. The average stress of thin film structures

Si-Ti/Pd/Pt	$Y_2O_3$		
Measured			Calculated
Stress	R	Thickness	Stress
(MPa)	(m)	(nm)	(MPa)
384	34.726	110	618.20
402	61.704	193	374.94
403	-85.524	410	-126.14
405	-168.400	460	-63.74
374	-16.060	1000	-334.16
399	-15.040	1000	-256.80

Experimental and calculated data are given in Tab. 1. Figure 3 shows a plot of the average stress of  $Y_2O_3$  wafers versus their thickness. The transition from tensile to compressive stresses takes place in  $Y_2O_3$  films with an increase of their thickness. The absolute values of intrinsic stresses are lower (by  $\approx 0.3$  GPa) in comparison with published data [5]. These results can be explained by the

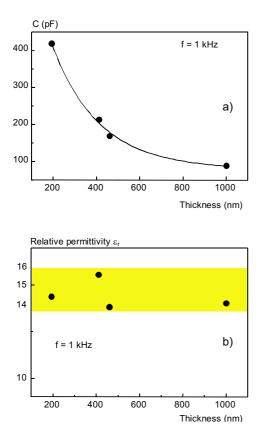


Fig. 6. Dependence of a) capacitance and b)relative dielectric permittivity on thickness of  $Y_2O_3$  thin films

relaxation of intrinsic stress during film growth due to self-heating of the substrate caused by RF diode sputtering.

Surface morphology of  $Y_2O_3$  thin films was observed using the Atomic Force Microscope (AFM). The AFM can image nonconducting as well as conducting surfaces. The AFM works recording the interatomic forces between its tip and surface atoms as the tip is scanned over the surfaces of the sample [4].  $Y_2O_3$  thin films have a polycrystalline structure (Fig. 4) and the size of grains on the whole surface is uniform and rises up with increasing of  $Y_2O_3$  thin film thickness (Fig. 5).

## 3.2 Electrical properties of $Y_2O_3$ thin film

As we described before, electrical measurements were made using a multilayered structure  $Ti/Pd/Pt-Y_2O_3-Al$ . The relative dielectric permittivity was determined from capacitance measurements

$$\varepsilon_r = \frac{C}{\varepsilon_0} \frac{d}{S} \tag{5}$$

were C is the measured capacitance of the multilayered structure,  $\varepsilon_0$  is the permittivity of vacuum, S is the area of the Al contact and d is the thickness of Y<sub>2</sub>O<sub>3</sub> film. The initial value of capacitance (419 pF) decreased exponentially with increasing Y<sub>2</sub>O<sub>3</sub> thickness (Fig. 6a). The calculated relative permittivity,  $\varepsilon_r \approx 15$ , was independent of the thickness (Fig. 6b) and its value is in good agreement with published data [9]. We can see from the dependence of the capacitance versus frequency (Fig. 7) that the capacitance of  $Y_2O_3$  thin films is relatively independent of frequency up to 100 kHz. The capacitance is also independent of the applied voltage in a wide range (±20V). The independence of  $\varepsilon_r$  of thickness, frequency and applied voltage demonstrates that relatively thin  $Y_2O_3$  films are very useful for dielectric separating layers.

Electrical cross-resistivity of  $Y_2O_3$  thin films was estimated by I - V measurements and its values are in the order of  $10^{11}\Omega m$ . The examined  $Y_2O_3$  thin films have shown a low leakage current, max. 0.4 nA at 100 V, which corresponds to electrical strength of  $2.5 \times 10^8$  V/m. The value of the breakdown voltage (destruction of  $Y_2O_3$  structure) was up to 100 V in all samples.

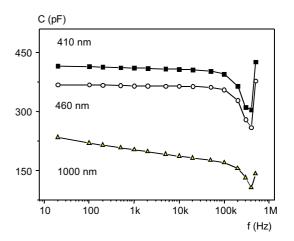


Fig. 7. Dependence of Ti/Pd/Pt-Y<sub>2</sub>O<sub>3</sub>-Al thin film structures capacity of frequency at different Y<sub>2</sub>O<sub>3</sub> thickness

### 4 CONCLUSION

The presented results confirmed a possible application of RF sputtered  $Y_2O_3$  thin films as an insulating layer in micro-electrochemical cells.  $Y_2O_3$  thin films are polycrystalline with a homogenous surface which consists of  $Y_2O_3$  grains. The grain sizes are different and comparable with corresponding thicknesses. In Tab. 2 the selected properties of  $Y_2O_3$  thin films prepared by RF sputtering with published data of  $Y_2O_3$  films are compared. Further investigations of these thin films open the way for their prospective applications in different domains of microsystem technology.

Table 2. The properties of  $Y_2O_3$  thin film prepared by RF sputtering compared with published data [2,6,7,9]

	Published Data	Our Results
Resistivity	$10^{11} - 10^{12} \Omega \mathrm{m}$	$\approx 10^{11} \Omega m$
Electrical intensity	$10^8 - 10^9 V/m$	$pprox 10^8 \mathrm{V/m}$
Relative permittivity	11 - 15	$\approx 15$
Young modulus	150GPa	$\approx 150 \mathrm{GPa}$
Intrinsic stress	$\approx 8 \mathrm{GPa}$	$\approx 0.3 \mathrm{GPa}$

## Acknowledgement

The presented work was supported by SK Grant VEGA 1/0168/03 of the Slovak Grant Agency and in part by the PPP - programme DAAD project 11/2001. We thank to Dr-Ing K.-H. Drüe, TU Ilmenau, as well as to Dr-Ing P. Kornetzky, IMMS Ilmenau, for their help in performing the electrical measurements.

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Received 12 December 2002

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