MECHANICAL BEHAVIOR AND THERMAL STABILITY OF EVA ENCAPSULANT MATERIAL USED IN PHOTOVOLTAIC MODULES

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The mechanical behavior and the thermal stability of an encapsulant based on ethylene-vinyl acetate (EVA) were studied. The EVA properties were verified at temperatures ranging from −70 °C to 500 °C. Thermogravimetry, differential scanning calorimetry and dynamic mechanical analysis were used in this study. It has been shown that the encapsulant has a good weight stability; however, the encapsulant passes through both a glass transition and a melting phase in the range of operating temperatures. The kinetic parameters of crosslinking were also analyzed. It is possible to achieve 65 % crosslinking at a temperature of 150 °C and a time of 5 minutes. The activation energy of crosslinking is 95.6 kJ/mol.

Key words: renewable energy resources, photovoltaic, EVA, encapsulant, glass transition, thermal analysis

1 INTRODUCTION

Renewable energy resources are an integral part of our lives. As one of these resources, solar energy does not function without reliable photovoltaic modules. Nowadays, publications concerning photovoltaic modules mostly deal with the manufacturing and optimizing of silicon layers [1, 2], rising efficiency of solar energy transformation ([3, 4] and many others) or ways to decrease manufacturing costs eg. Espinosa et al [5], Kalowekamo and Baker [6]. Little interest is paid to the reliability of these modules [7, 8]. Considering that manufacturers usually guarantee module lifetime at the least for 20 years, it is necessary to take this lifetime into account and focus on used materials and performance. One key component of photovoltaic modules that influences total reliability is the encapsulant material [9]. Therefore, the main aim of the paper is to analyze mechanical properties together with the thermal stability of an ethylene-vinyl acetate (EVA) film widely used for encapsulation of photovoltaic modules.

2 BACKGROUND

The typical photovoltaic module consists of several main layers (see Fig. 1). The part that attracts the most attention is the solar cell itself. The cell is notably brittle under common environmental exposure; therefore, it is necessary to protect the cell during its operation [10, 11]. It is obvious from Fig. 1 that the solar cell is shielded on the front from mechanical stress (ie, stress during transport, installation or operation stress — wind blast, hailstones or dust influence) by the protective glass sheet. On the backside, the cell is protected with a protective sheet made mostly of plastics.

3 EXPERIMENTAL PROCEDURE

3.1 Materials

A commercially available encapsulant (VISTASOLAR®, ETIMEX Solar GmbH, Dietenheim, Germany) based on
Mechanical Behavior and Thermal Stability of EVA posed to a linear heating rate of 5°C/min starting from −70°C and increasing to 200°C in a dry-air atmosphere. Circle-shaped samples were prepared by cutting the EVA film for use in all of the aforementioned methods.

4 RESULTS AND DISCUSSION

4.1 Preliminary measurements

First, a series of preliminary measurements on crosslinked and uncrosslinked EVA foil samples were performed. TG analysis was used to examine the weight stability of crosslinked EVA and to determine the approximate vinyl acetate content. The thermogravimetry results are presented in Fig. 2. The analysis demonstrated the good weight stability of crosslinked EVA over temperatures ranging from 25°C to 90°C (weight loss of 0.14%). This result confirms that the crosslinking was performed correctly, as well as a good future weight stability in the interval of higher operational temperatures.

Similar results were obtained, e.g., by Agroui et al. [12]. It has also been shown by TG that the EVA supplied contains 25.5% of vinyl acetate (where residue at the end of the measurement has been considered in the calculation). A measured content of vinyl acetate 32.5% is presented at nitrogen atmosphere by Klemchuk et al. [9].

A kinetics analysis of the crosslinking process was performed to understand crosslinking dynamics and for a contingent optimization of the crosslinking process. Measurement and calculation of Arrhenius kinetic parameters were performed in accordance with ASTM E698E-05 [15]. First, the crosslinking reaction of uncrosslinked EVA foil was recorded at different heating rates by DSC (Fig. 3), and temperatures at which the reaction peak maxima occur are subsequently plotted as a function of their respective heating rates and kinetic values (activation energy and pre-exponential factor) calculated from the peak temperature-heating rate relationship are used to predict reaction half-life at a selected temperature.

The percent of conversion as a function of time at different temperatures (120-190°C) is plotted in Fig. 4. It is obvious that the crosslinking reaction is notably fast.

Agroui et al. [13] recommend a minimum acceptable conversion level (EVA gel content) of 65% with reference to work performed at Springborn Laboratory. Manufacturers of photovoltaic modules follow the same rule, and 65% conversion is considered to be satisfactory. This level is marked in Fig. 4 and is achieved in 5 minutes at a temperature of 150°C, as recommended in the material sheet. Considering a different approach for crosslinking (crosslinking in the DSC apparatus), the time is comparable to that specified in the material sheet. The activation energy of EVA crosslinking was calculated as 95.6 kJ/mol with a pre-exponential factor $11.12 \, \text{l/min}$ and a 60-min half-life of 109.3°C. The $E_a$ value is consistent with that (91-107 kJ/mol) reported by Bianchi et al. [16].
It should be noted that temperature and time of crosslinking are just two of several parameters for determining the proper lamination of a photovoltaic module. The fabrication pressure during lamination also plays an important role. Bubbles can behave similar to optical lenses when the lamination is not properly performed. Consequently, bubbles in interaction with sun rays can cause the destruction of solar cells [8].

4.2 Dynamic mechanical analysis

Thermogravimetry demonstrated good weight stability over higher operating temperatures. Solar cells can also be exposed to extremely low temperatures (in some cases, even approximately −30 to −40°C), particularly during the winter season. At such low temperatures, ethylene-vinyl acetate reaches the glass transition temperature [14], and the elastic material becomes solid and notably brittle. Hence, it is very important to monitor the glass transition temperature and the mechanical properties of the EVA film by dynamic mechanical analysis, as it is considered to be the most accurate method for this purpose [17, 18].

DMA is a technique in which the deformation of a sample under oscillatory load is measured as a function of temperature, while the sample is subjected to a controlled temperature program. DMA is able to characterize and interpret the mechanical behavior of the material. In short, DMA consists of the application of an oscillating force to a sample and observation of the material in response to that force [19, 20]. DMA allows division of the material’s viscoelastic response into the two components of the complex modulus ($E^*$): 1) a real part represented by the storage modulus $E'$ [MPa] (ability of the material to return or store energy), and 2) the imaginary part, often called the loss modulus $E''$ [MPa] (ability to lose energy). This separation describes two independent processes in the material, specifically, elasticity and viscosity [21]. The phase angle between those module is defined as the loss factor, $\tan \delta$, and equates to

$$\tan \delta = \frac{E''}{E'}.$$  \hspace{1cm} (1)

The DMA results are presented in Fig. 5, where both the crosslinked and the uncrosslinked samples of tested EVA samples are shown. The module, $E'$, $E''$, and loss factor, $\tan \delta$ were obtained as functions of temperature during the evaluation.

As obvious from Fig. 5, both module and the loss factor have been changing during the measurement. These changes are related to glass transition, which can be characterized by the glass transition temperature ($T_g$). The DMA can generally provide three values of the glass transition temperature, which can be analyzed either as a peak maximum of loss modulus ($E''$), as a peak maximum of loss factor ($\tan \delta$) or as an onset temperature for the decrease of the storage modulus ($E'$). Each of these temperatures has physical merit and interpretation. As Foreman et al [17] mention, in the case of the storage modulus, the onset temperature defines the temperature at which the material strength will begin to decrease such that the material may no longer be able to bear a load without deformation. The peak maximum of the loss modulus represents the temperature at which the polymer material undergoes the maximum change in mobility.
of the polymer chains. The peak of the loss factor characterizes the damping characteristics associated with a material.

As Fig. 5 also illustrates, there is a marked increase of the storage modulus (with values almost twice as high) due to crosslinking. Additionally, a slight shift of all analyzed temperatures toward more negative values was observed. The onset temperature for a decrease in the storage modulus, which is the most important property of photovoltaic modules from an operational point of view, is stable at approximately $-40^\circ C$ after crosslinking. This temperature is also often declared by EVA film manufacturers to be the thermal minimum for application. The eventual mechanical stress the photovoltaic module experiences (e.g., wind blasts and heavy snow cover) at very low temperatures causes measurable changes in the inner structure much earlier. These changes are expressed by the maximum of the loss factor, the range of which (from higher to lower temperatures) means that the EVA film begins to transform from its flexible state into a brittle state and is no longer able to respond to the mechanical energy caused by the eventual mechanical stress of the module. This energy is subsequently changed in the inner structure of the material into thermal losses that are detected by the high value of tan $\delta$. In the case of the crosslinked EVA, the maximum value of tan $\delta$ was observed at a temperature of $-16.9^\circ C$.

4.3 Differential scanning calorimetry

The crosslinked sample of copolymer EVA was also analyzed by differential scanning calorimetry to determine the melting temperatures. The results are shown in Fig. 6.

It is obvious that from $30^\circ C$, the DSC recorded the beginning of two overlapping endothermic peaks (with peak maxima at $45.6^\circ C$ and $66.7^\circ C$). This phenomenon is the melting of two populations of crystalline perfection. With reference to Agroui et al [12], the lower of those two temperatures refers to melting of imperfect, small crystallites, and this melting occurs due to the integration of vinyl acetate into the polyethylene structure. By comparison, the higher temperature refers to the melting of larger and more regularly formed crystallites in the polyethylene.

5 CONCLUSION

Thermogravimetry demonstrated a good weight stability for crosslinked EVA over temperatures ranging from $25^\circ C$ to $90^\circ C$. DMA marked the increasing storage modulus due to crosslinking. The onset temperature of the storage modulus is approximately $-40^\circ C$ after crosslinking, but measurable changes in the inner structure are first observed much earlier. The glass transition temperature (from the tan $\delta$ peak maximum), in the case of crosslinked EVA, was observed at a temperature of $-16.9^\circ C$. The obtained results show that the EVA film is getting more brittle (i.e., more sensitive to mechanical stress when moving toward lower temperatures). Conversely, at higher temperatures, vinyl acetate crystallites begin to melt, even temperatures as low as $46^\circ C$, and polyethylene crystallites begin to melt at $67^\circ C$. These findings are not desirable from an operational point of view. Due to the instability of the encapsulant film, there is a possibility of delamination during operation, and this effect can directly threaten the solar cell itself, and thus the entire photovoltaic module [8]. Although several studies suggest there are more suitable encapsulant materials, e.g., silicon-based materials [14, 22], ethylene copolymers based on acrylic acids and acrylate [23], EVA films remain dominant in the photovoltaic industry.

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References

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